



**GSFC • 2015**

# **Continued Water-Based Phase Change Heat Exchanger Development**

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Mezzo Technologies Inc.



# Overview

- Why use Phase Change Material Heat Exchanger's (PCM HX's)?
- Prior PCM HX Development and Testing
- Full-Scale Design
- Prototypic Freezing and Thawing
- Unit A and Unit B Testing Summary
- Subscale Design and Testing Summary



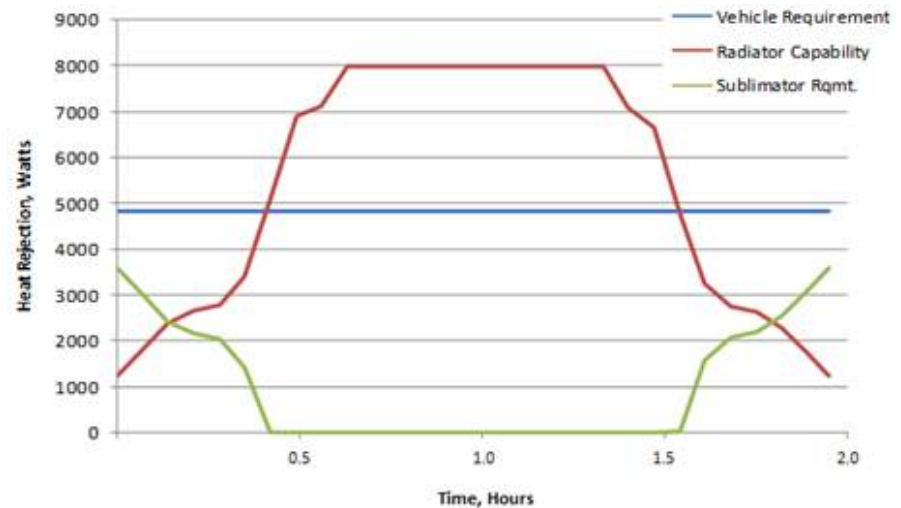
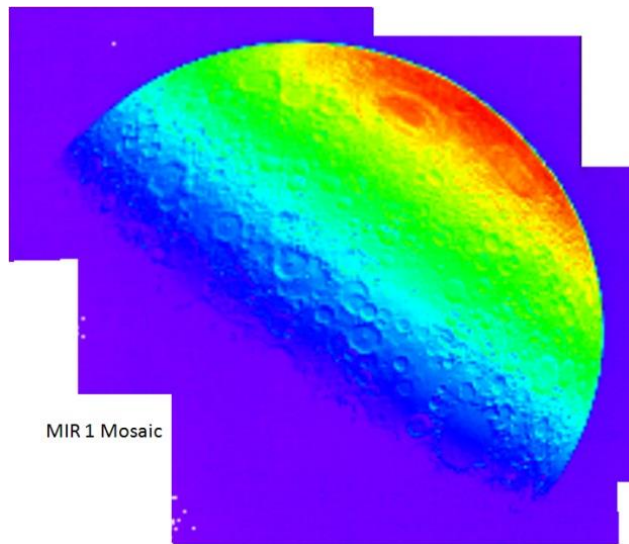
# **WHY USE A WATER-BASED PCM HX?**



# Why Use Water as a PCM?

- In cyclical heat load environments, a Supplemental Heat Rejection Device (SHReD) is required
  - Typically, accomplished through evaporators, sublimators, or Phase Change Material Heat Exchangers (PCM HX)
  - PCM's act a thermal battery and do not use a consumable
- Wax PCM is baseline for the Orion Spacecraft, but water is being investigated
  - Water has significantly higher latent heat of fusion than wax (333 kJ/kg vs. 163 kJ/kg)
  - Significant mass and volume savings possible

Problem: Water expands ~10% when frozen





# **PRIOR PCM HX DEVELOPMENT AND TESTING**



# Why Use Water as a PCM?

PCM HX  
Development

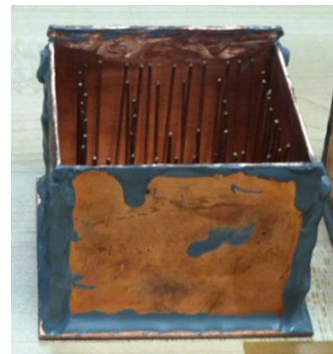
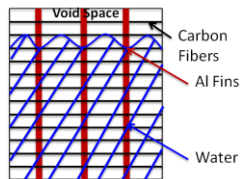
Energy  
Sciences  
Laboratory

Bench-Top  
Testing

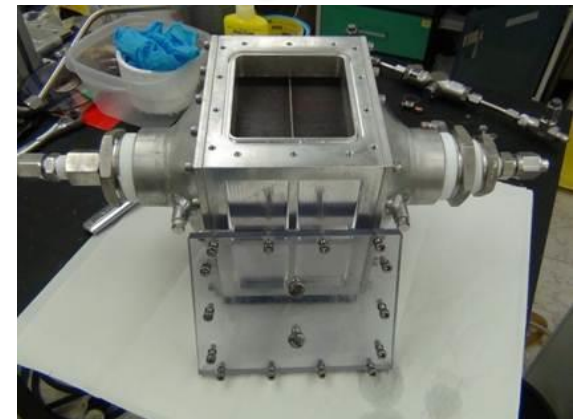
Mezzo  
Technologies



*Ice Spike Formation Comparison in  
SHRIMP*



*Copper Coupon*

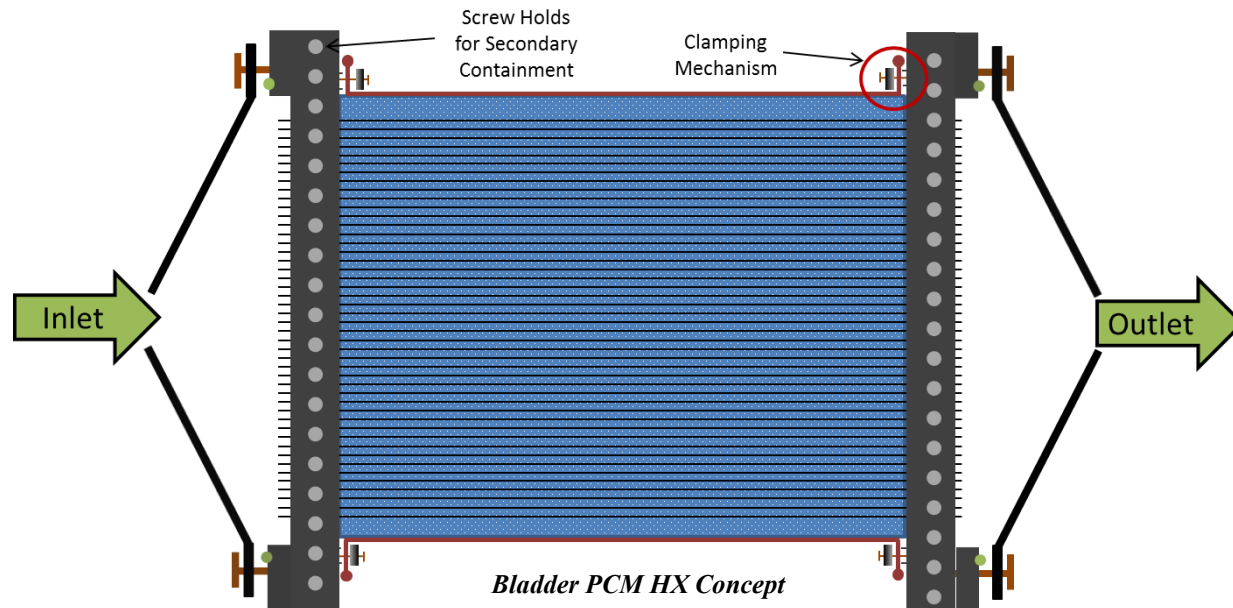


*Mezzo Technology HX*



# Learning Outcomes from Historical Testing

- Providing extra void space may not necessarily lead to the development of a successful HX as void space will not necessarily be known in microgravity
- Use of “ice spike distribution” through inside-out freezing or uniform freezing should be pursued for future development
- Use of a bladder is feasible to implement with a water-based PCM HX





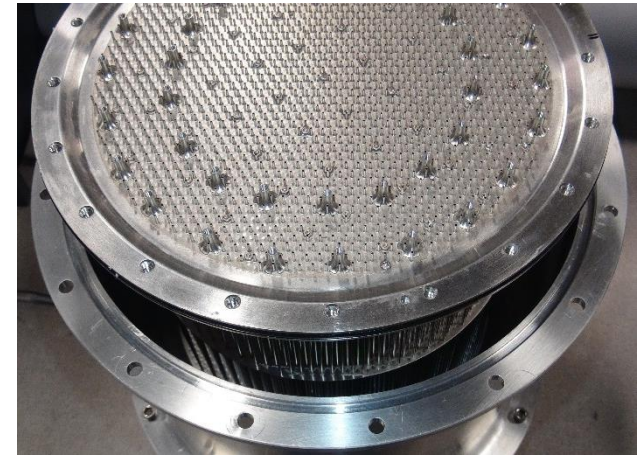
# **FULL-SCALE DESIGN AND DEVELOPMENT**



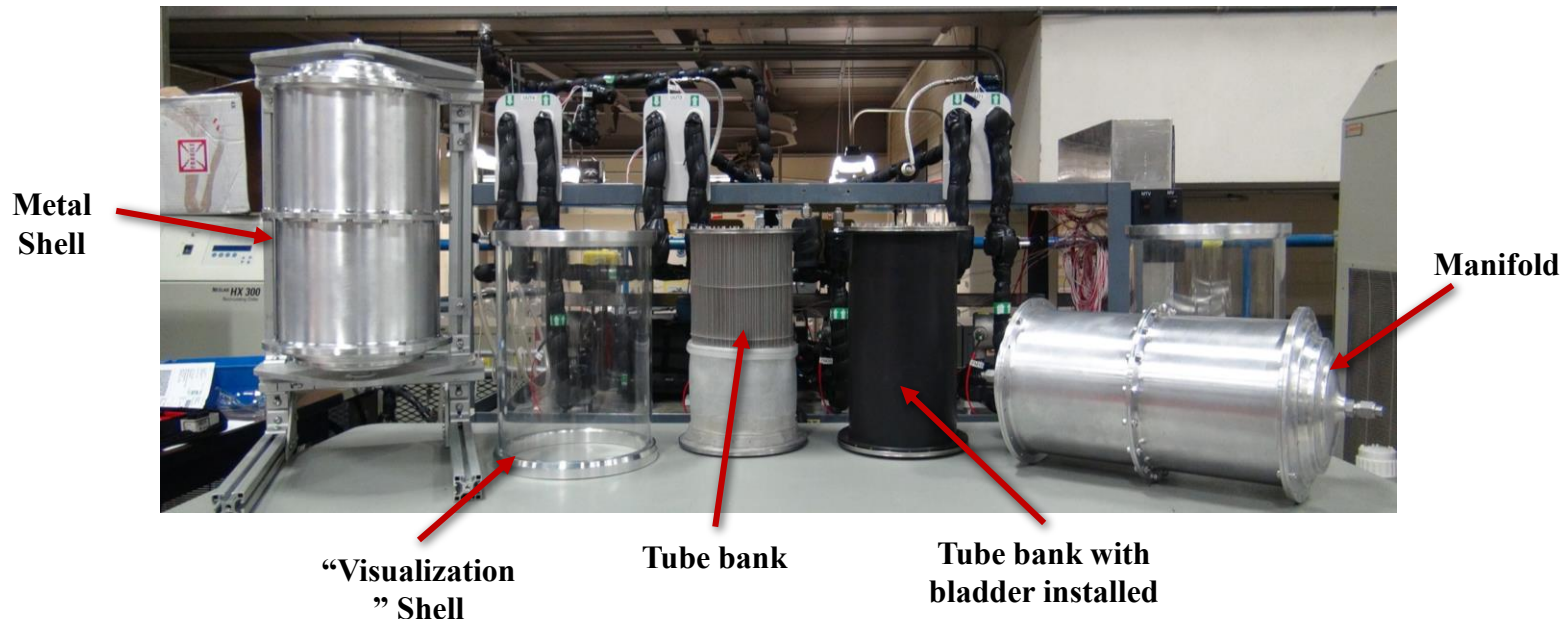


# Full-Scale Design and Development

- 2 Orion-like full-scale PCM HX were designed and constructed through a SBIR Phase II with Mezzo Technologies
  - 3,700 kJ energy storage
- Each unit consists of 3 main components
  - Tube bank
  - Manifolds
  - Metal or “visualization” shell
- 12 kg of metal and 11.1 kg water
- Thermal analysis from Mezzo showed that it is possible to freeze/thaw in 90/30 minutes given sink temperatures and associated PCM inlet temperatures and flow rates



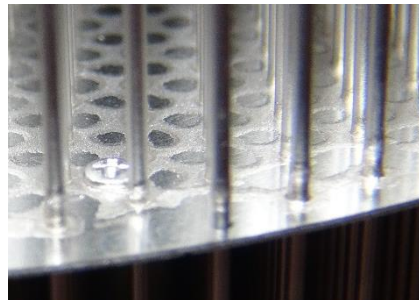
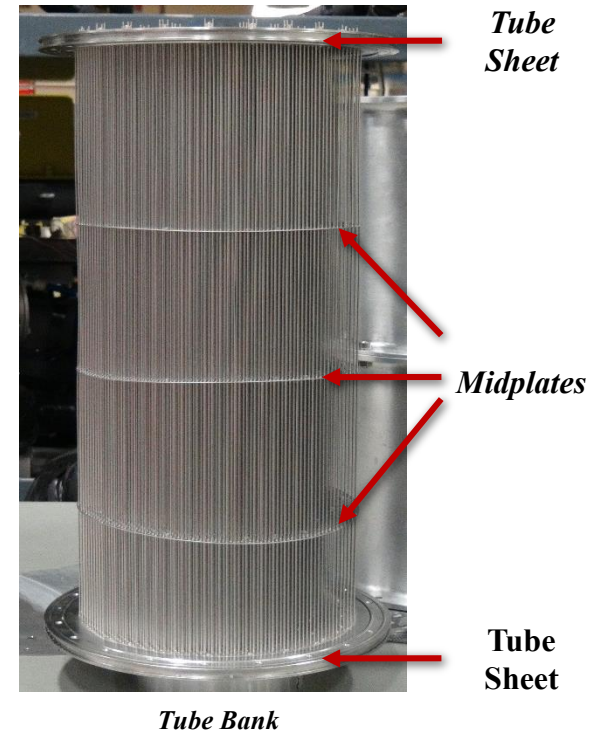
*Tube Bank Being Installed into Shell*



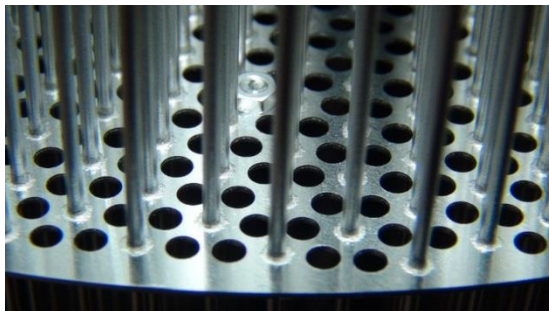


# Full-Scale Design and Development (Cont.)

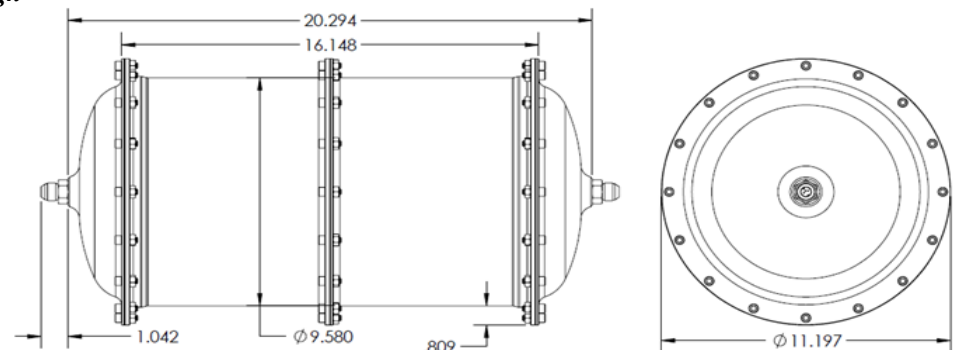
- Tube bank consists of 1,420 tubes
  - OD 0.042", ID 0.035", wall thickness 0.0035"
  - 10% greater concentration in the center
  - Tubes brazed to tube sheets and midplates
- 2 Units constructed (EDU A & EDU B)
  - Units are essentially identically differing only by their midplate
  - Unit A: No holes in midplate
  - Unit B: Holes in midplate
- Viton GLT bladder manufactured through injection molding



*Unit A Midplate Design*



*Unit B Midplate Design*



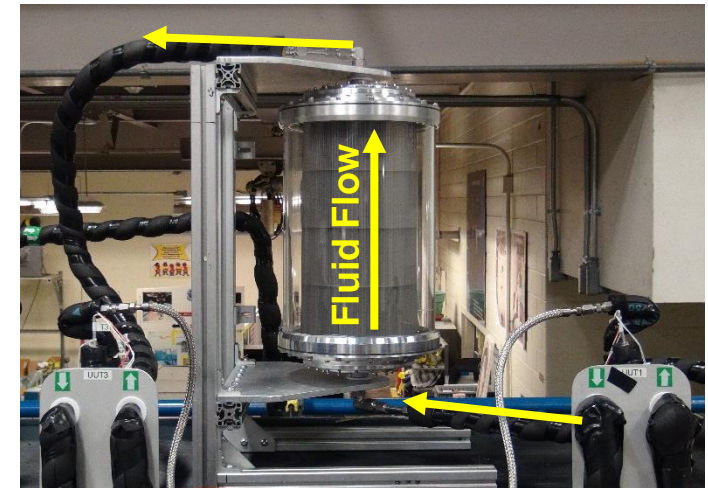


# PROTOTYPIC FREEZING AND THAWING



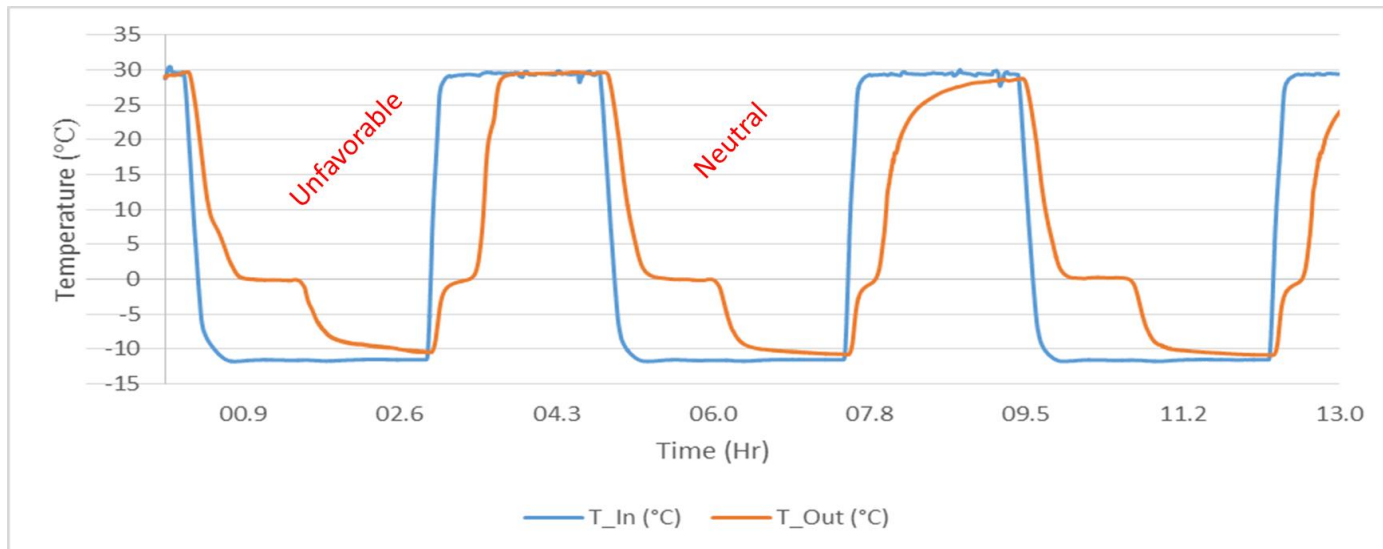
# Test Set-Up

- Tested on RIP test stand at JSC
- 3 orientations tested
  - Favorable, unfavorable, neutral
- 50/50 PGW used as a working fluid with inlet and outlet temperatures of -12C to 30C controlled by chiller carts
- Transient testing also tested
- Bladder filled 100% with degassed water and 0% void space
- Goal was to achieve 100 cycles without failure



*Favorable Testing Fluid Flow*

*Normal Freeze/Thaw Cycle Profiles*

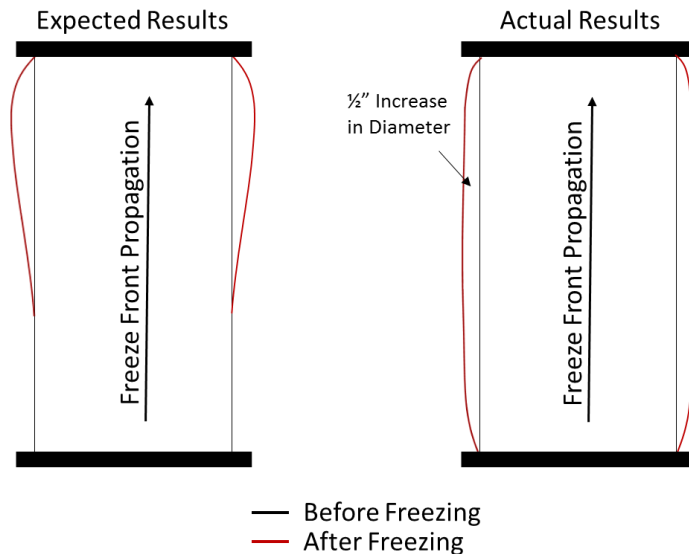






# Test Set-Up

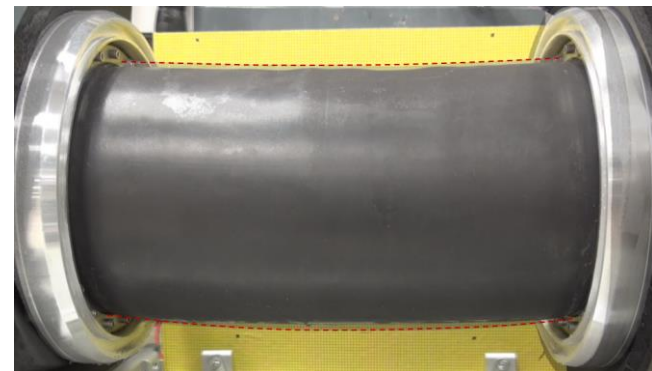
- Bulge near outlet was expected to be observed during freezing but no bulge occurred
  - Due to bladder flexibility
  - Max expansion of  $\sim 1/2''$  (estimated at  $3/4''$ )
  - Midplates did not have a noticeable effect on ice spike formation



*Image Comparison: Favorable*



*Image Comparison: Unfavorable*



*Image Comparison: Neutral*



# Prototypic Thaw Cycle

- Thawing did not occur as predicted
  - Hypothesized that bladder would simply return to its original position,
  - Bladder was pressed against tube bank because of decreased internal pressure due to melting water and corresponding decrease in volume
  - Caused significant bending in tubes around perimeter of the HX



*Fully Frozen*



*10 min*



*15 min*



*25 min*



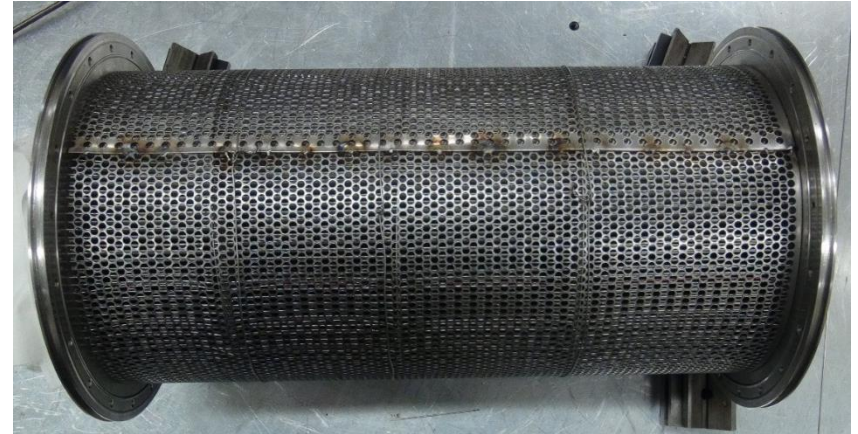
*Unit A Bent Tubes Post-Test*



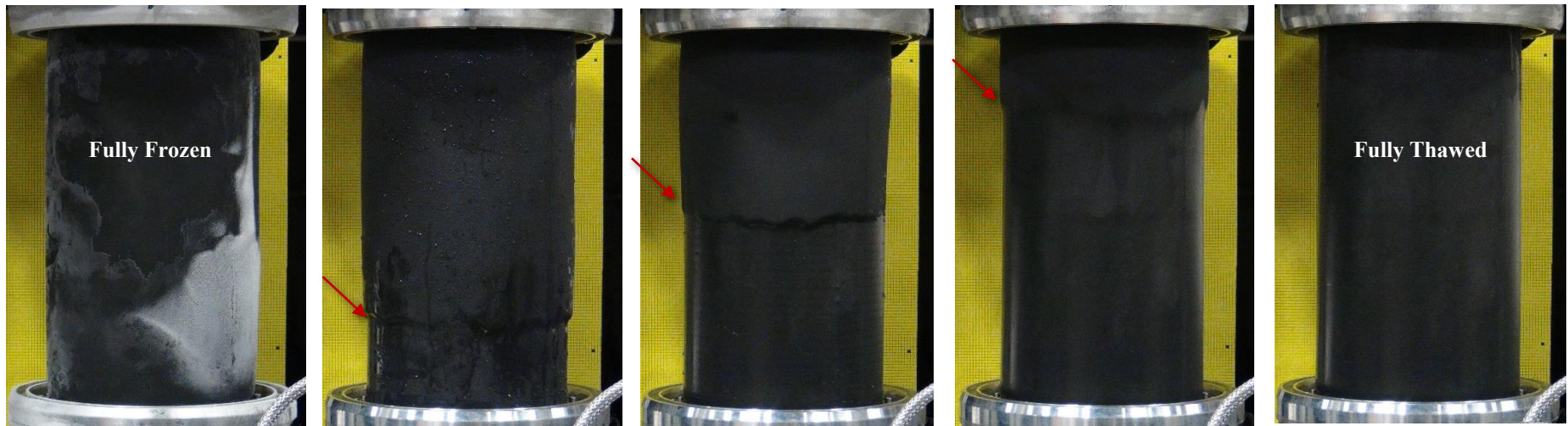


# Perforated Sheet Addition

- To prevent tubes around the perimeter of the HX from bladder compression, a stainless steel perforated sheet was cut, rolled, and spot welded onto the tube bank core
- Testing resumed after sheet was in place



*Perforated Sheet Installed*



*Thawing Progression with Perforated Sheet Installed*



## **UNIT A AND UNIT B TESTING SUMMARY**

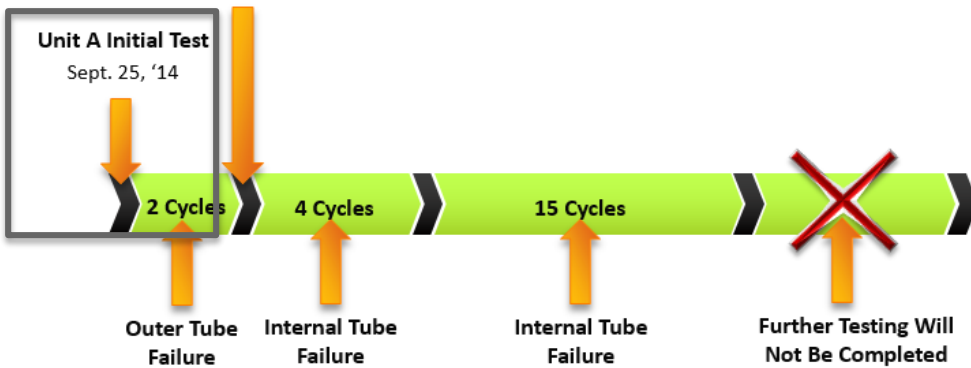




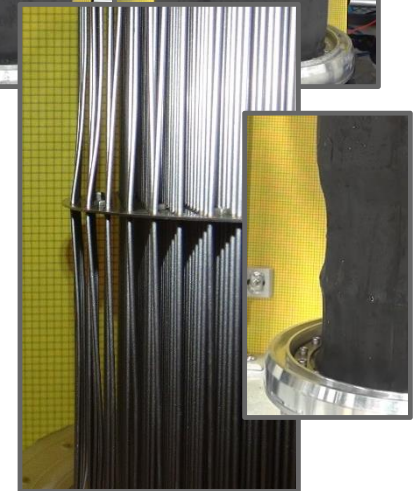
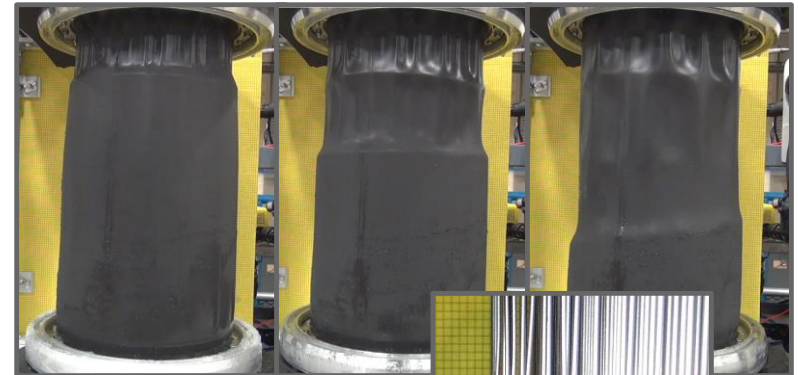
# EDU A&B Testing Summary

Perforated Sheet  
Installed

Unit A Initial Test  
Sept. 25, '14

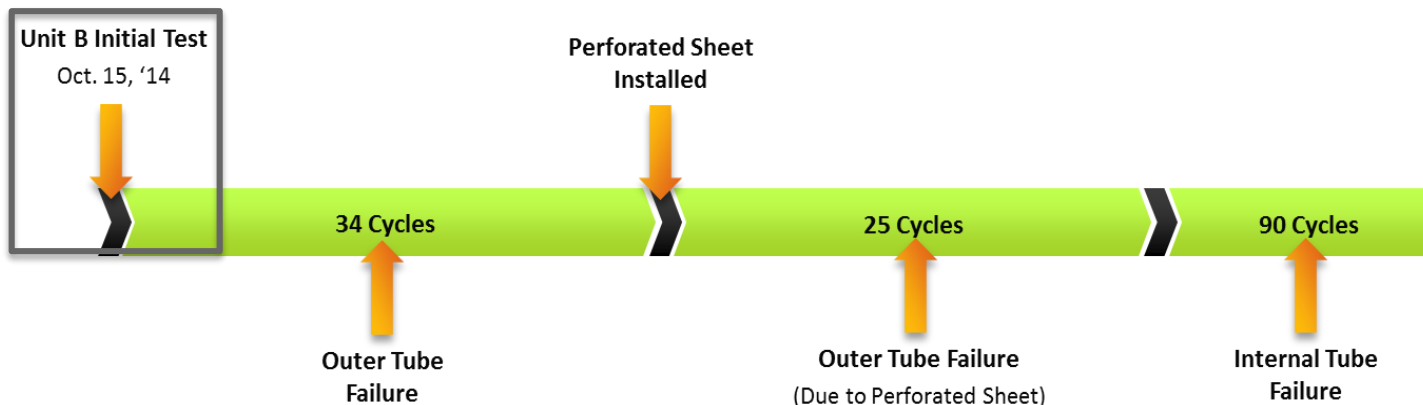


- Freeze and thaw tests were done on both EDUs with the Viton® bladder
  - Upon freezing the unit, the ice caused the bladder to expand as expected
  - Upon thawing, the bladder compressed onto the tubes due to the contraction of the water



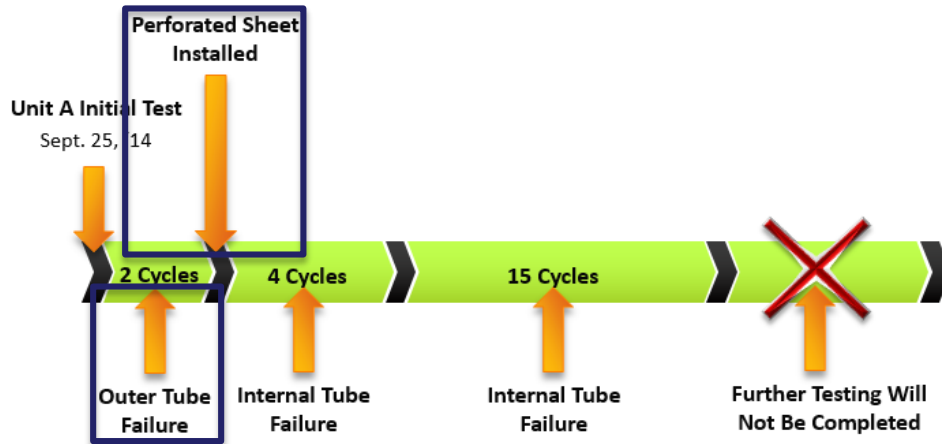
Unit B Initial Test  
Oct. 15, '14

Perforated Sheet  
Installed





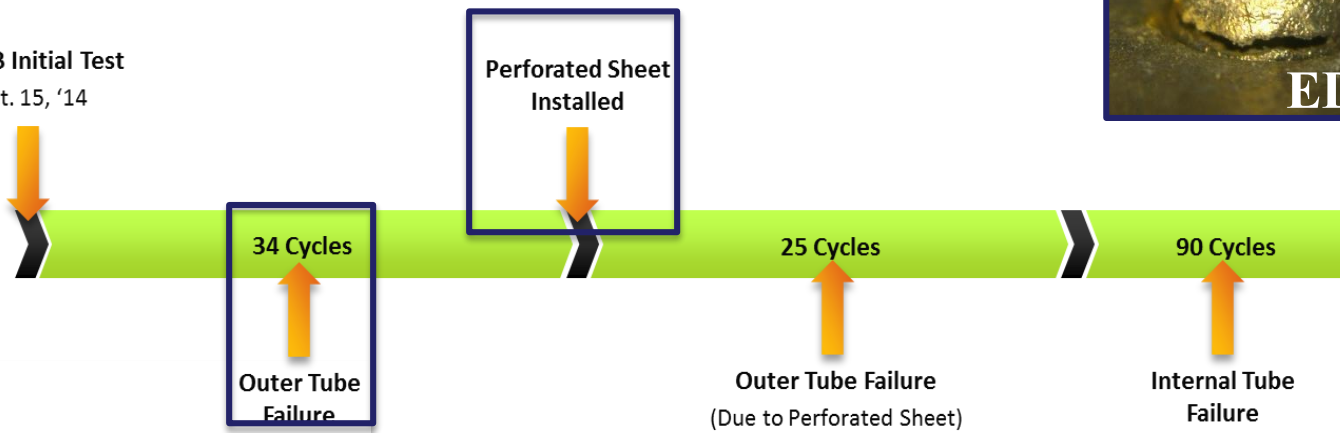
# EDU A&B Testing Summary



- Due to multiple compressions cycles of the bladder on to the perimeter tubes, a failure of an outside tube eventually occurred on both units
- A perforated sheet was wrapped around the tube core of the HX to protect from the compression

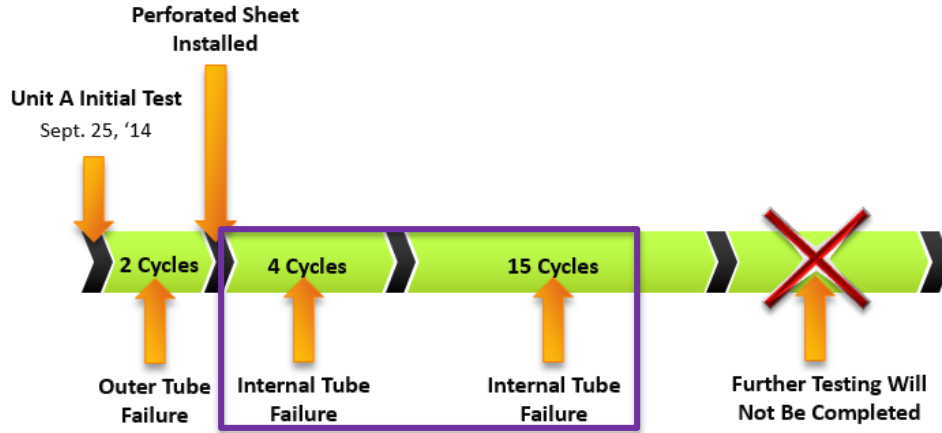


**Unit B Initial Test**  
Oct. 15, '14

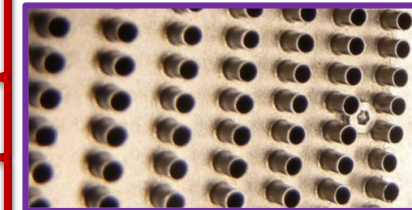
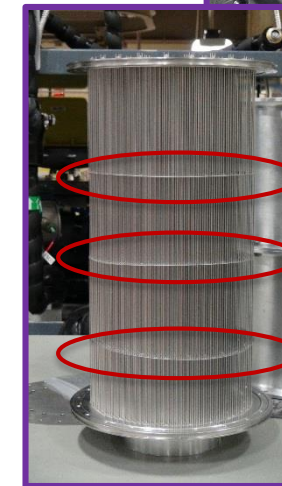
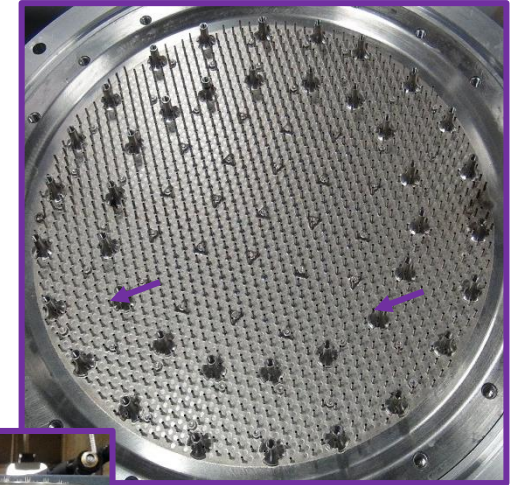




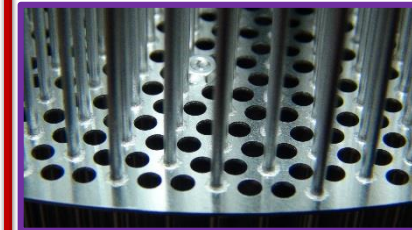
# EDU A&B Testing Summary



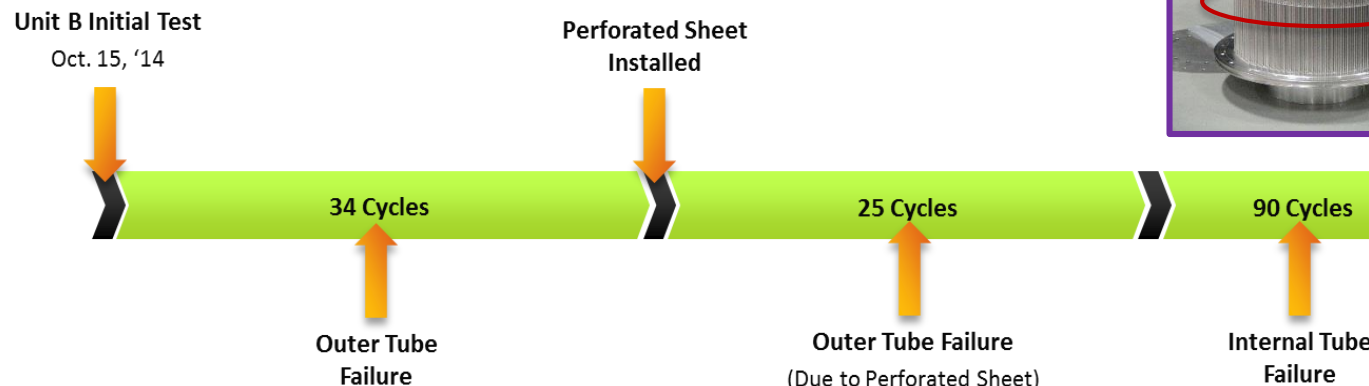
- Two internal tubes failed on EDU A
  - EDU A is the HX without perforated midplates
- The failure was hypothesized to be directly related to the freeze and thaw of the water on the inside of the HX
  - Water became hydraulically locked at midplate locations and did not have a path between various sections of the HX, causing pressure to be placed on a tube



**EDU A**



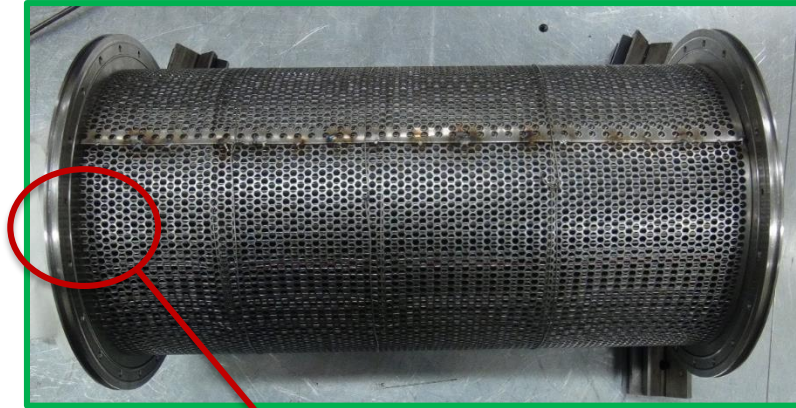
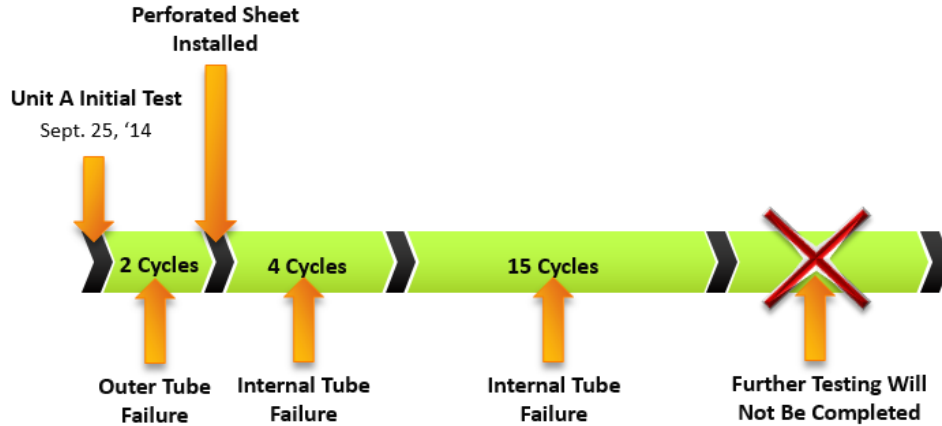
**EDU B**



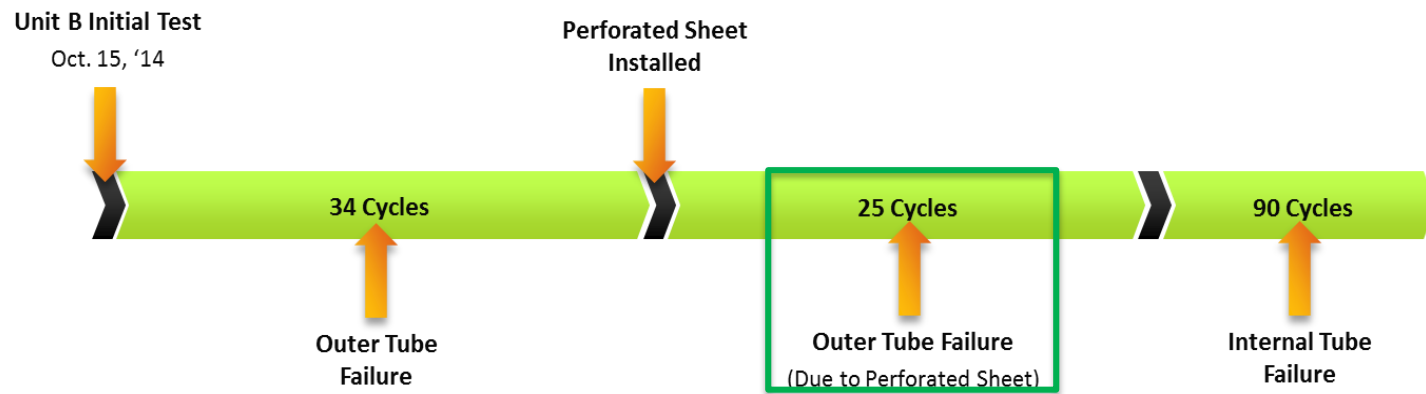
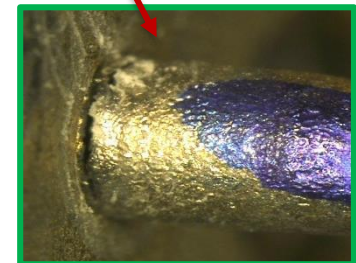
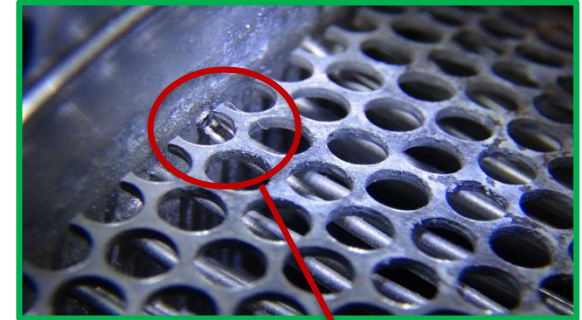




# EDU A&B Testing Summary

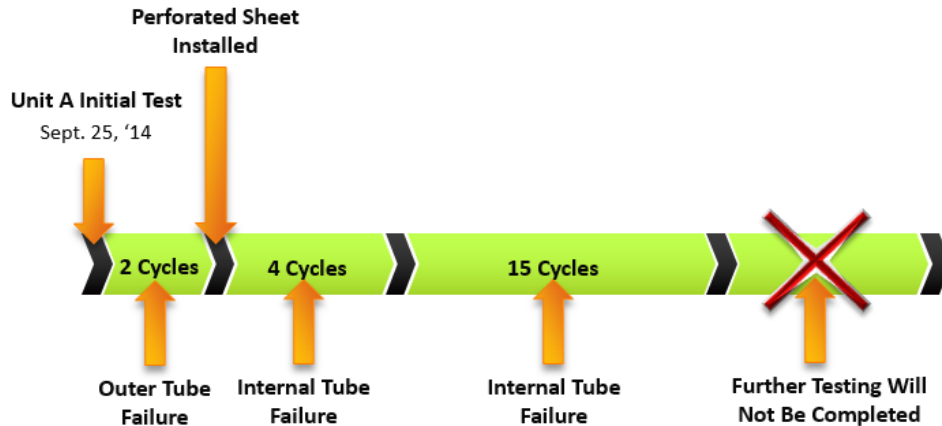


- During testing of Unit B, the bladder compressed onto the outer perforated sheet (meant to protect the outer tubes)
  - This caused the sheet to press against one of the tubes causing it to crack
- The tube was fixed and the perforated sheet was reinforced along the two edges to ensure this would not happen again



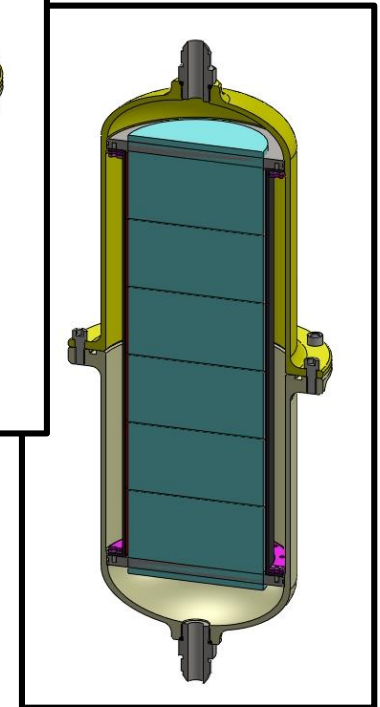
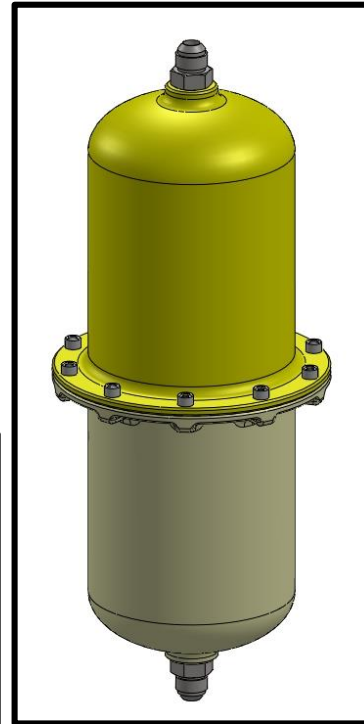
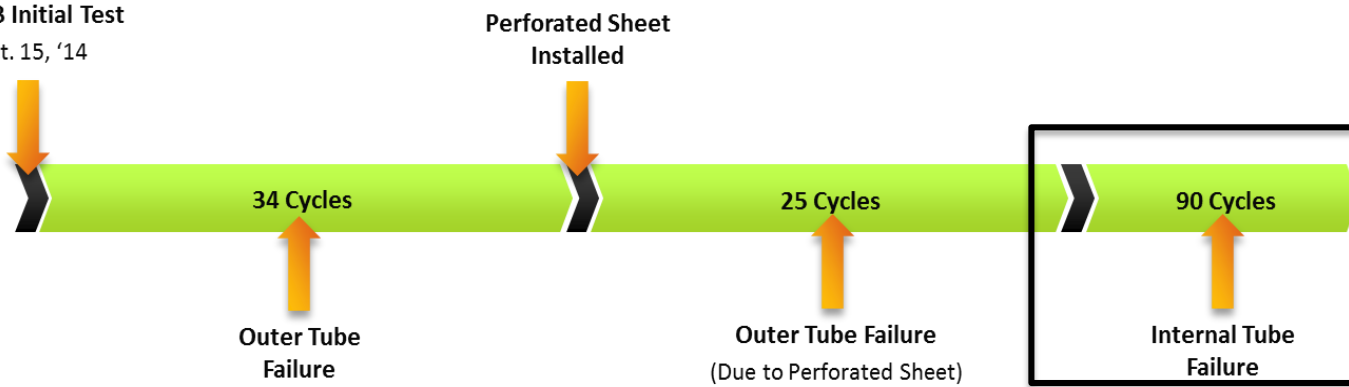


# EDU A&B Testing Summary



- Completed an additional 90 cycles on EDU B before an internal tube failed
- Location of failure could not be clearly identified during leak checking and tube sheet deformed during these tests so no further testing could be completed
- Continued with sub-scale PCM design and development using EDU B midplate design and lessons learned from testing EDU A and B

**Unit B Initial Test**  
Oct. 15, '14





# **SUBSCALE DESIGN AND TESTING SUMMARY**



# Subscale Design

- Subscale PCM HX is a “cookie-cutter” of the full-scale unit
  - Approximately 4” in diameter and 10” long (full scale unit is 8.75” diameter and 16.1” long)
  - Designed to meet size requirements of ISS PCM HX Demonstration Loop and Orion pressure requirements
- Applied EDU A/B lessons learned to subscale unit including
  - Decreased aspect ratio
  - Use of perforated sheet and associated retaining ring
  - Use of more midplates
- Major differences between full-scale and subscale units include
  - Increased tube diameter
  - Epoxied not brazed to reduce uncertainty of braze process



*“Cookie Cutter” of Full Scale Unit*



*Subscale Unit Components*

<u>Characteristic</u>	<u>Full-Scale Unit</u>	<u>Subscale Unit</u>
Outer Diameter (in)	0.042	0.058
Tube Wall (in)	0.0035	0.0058
# of Tubes	1461	324

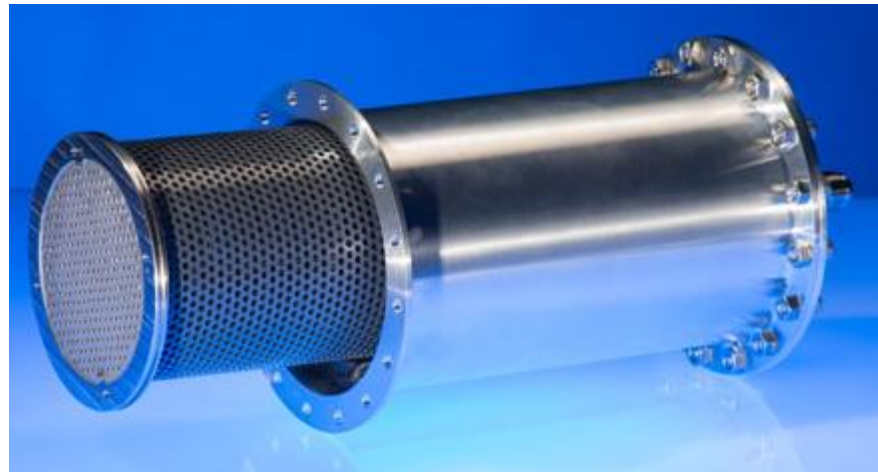


# Subscale Testing Outcomes

- Testing with approximately the same flow rate per tube area as full scale unit
  - 85 lbs/hr for subscale unit verses 235 lbs/hr for full scale unit
  - Allows for scalability between full-scale and subscale units
- No major differences noticed between full-scale and subscale freeze/thaw cycling
  - Bladder expands evenly over length of HX and perforated sheet protects HX core during thawing
- 150 successful cycle completed as of July 14th!
  - 40 favorable, 21 neutral, 89 unfavorable cycles
- 1 minor testing issue
  - During cycle 19, the water fill screw developed a very minor leak which was observed in the temperature time data.
  - O-ring grease was added to threads and o-ring and testing resumed
  - No leaks or failures since leak was fixed



*Tubes Inserted into Midplate*



*Subscale Core Inserted Into Shell*





**QUESTIONS?**